

# Beam Dynamics in Induction Linacs\*

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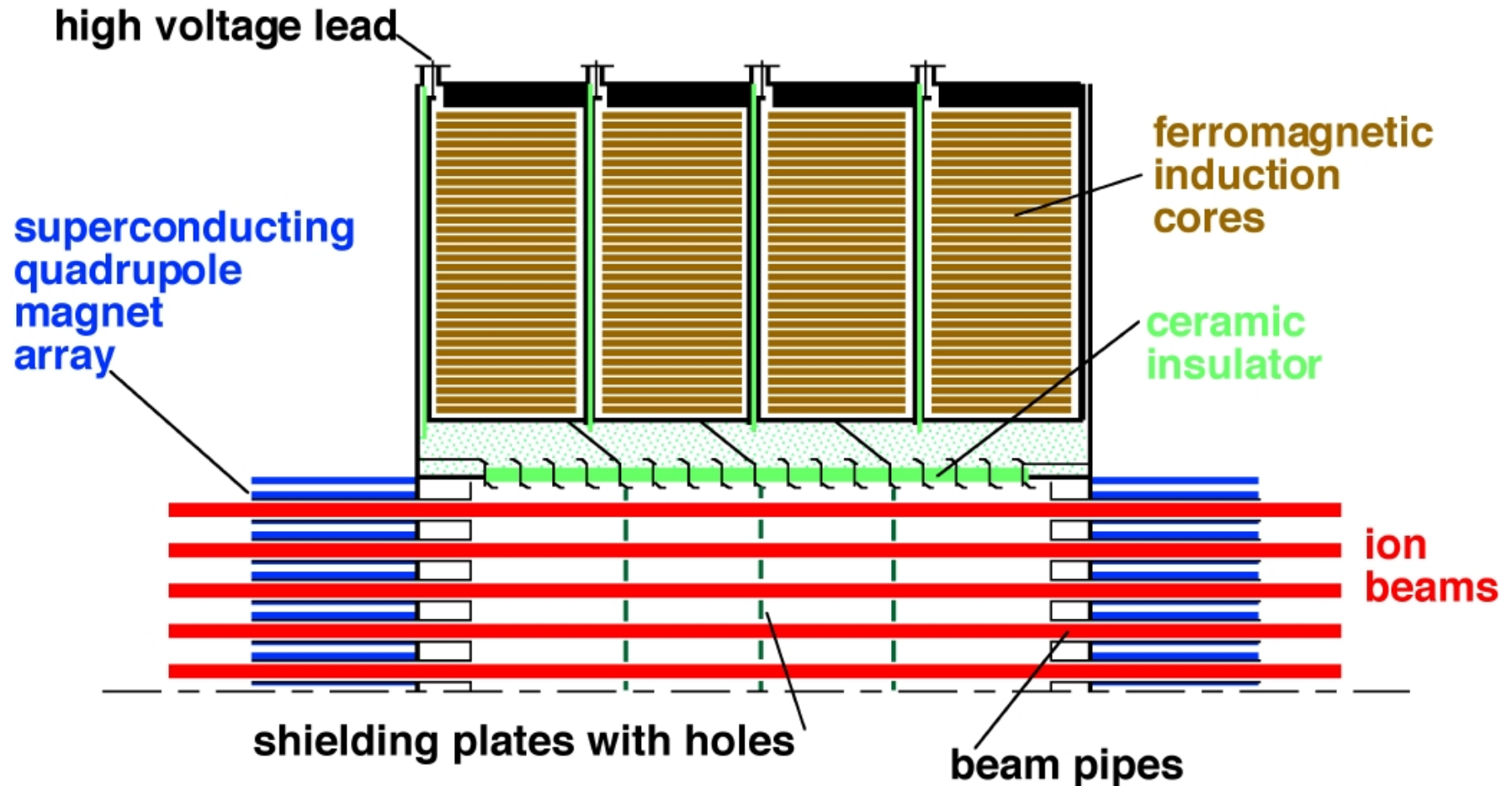
Induction Linac Features  
Beam Dynamics Overview  
Choice of Transport Lattice  
Longitudinal Stability

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The Heavy Ion Fusion Sciences Virtual National Laboratory



# In a Heavy Ion Fusion driver, ~100 beams are accelerated in tandem through a series of induction cells



*The beams interact with each other through EM fields: deflections, longitudinal inductive forces, and “loading” of the power source must be controlled.*

# Linear Induction Accelerators (LIA)

- Pulsed power circuitry puts an electric field directly on an acceleration gap:  
Charge in capacitor  $\rightarrow$  Switch  $\rightarrow$  Field on gap
- An induction core temporarily prevents the short to ground  
Gap voltage x pulse duration = (Longitudinal core area) x (core flux swing)  
example:  $200\text{kV} \times 1.0\mu\text{s} = .2\text{m}^2 \times 1.0\text{T}$
- Capacitor Energy  $\rightarrow$  Beam + Core heat + Refection
- The beam's return current flows through the pulsed power circuitry and induces a reverse field in the gap
- If refected energy can be recovered in the capacitor electrical efficiency can be high, e.g.  $\approx 50\%$  for  $I_{\text{beam}} \approx 1.0\text{kA}$

- Unlike an rf linac, the accelerator cavity/gap is not driven at a resonance. This allows for large aperture and high current, but with more complicated beam dynamics.

- The main experience so far:

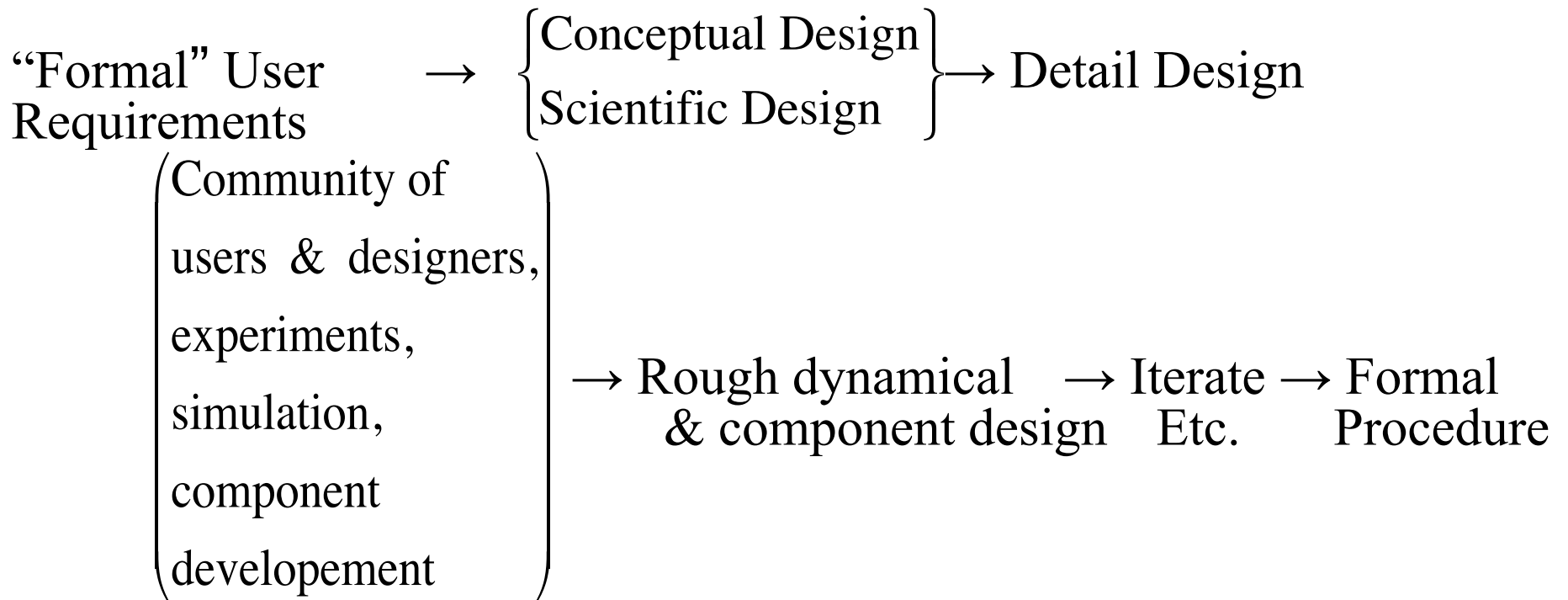
Electron LIAs for radiography	DARHT	$\left\{ \begin{array}{l} 20 \text{ MeV} \\ 1.0 \text{ kA} \end{array} \right.$
beam weapons	ATA	$\left\{ \begin{array}{l} 50 \text{ MeV} \\ 10 \text{ kA} \end{array} \right.$
fel & misc	ETA	$\left\{ \begin{array}{l} 5 \text{ MeV} \\ 1.0 \text{ kA} \end{array} \right.$
Ion LIAs for WDM and fusion exps.	NDCX II MBE4	$\sim 1 \text{ MeV Li}^+$ $\sim .4 \text{ MeV K}^+$

- Light Ion Fusion used pulsed power applied to a single or few gaps - very different from HIF (very high ion currents)

- Electron LIAs have used solenoids for transverse confinement. Longitudinal confinement is not needed because  $v = c$ .
- The main dynamical issue for electron LIAs has been the Beam Breakup Instability (BBU), a transverse hose-like motion driven by interaction with the accelerator modules
- Beam dynamics in HIF-LIAs is different from electron LIAs:
  - BBU is probably not significant
  - Transport is by magnetic quadrupoles, esp. for multiple beams
  - Longitudinal control is a critical issue
  - Beams must be very cold in both transverse and longitudinal directions (low emittance) to focus on target

# Accelerator Dynamics Design (e.g. for HIDIX)

There is a formal procedure, but a reverse informal “rough design” proceeds it and must be sound:



End-to-end dynamical model needed:

All known dynamical features included

All known issues resolved

Detailed component models for dynamics

This activity can guide research programs

## Some dynamical considerations

Design of transport systems with multibeam interactions - halos?

Vacuum in acceleration gaps -  $10^{-8}$  torr good enough?

Beam loss - activation, magnet operation,  $e$  cloud

Steering - all beams separately?

Alignment - all beams separately?

Diagnostics - all beams separately?

Longitudinal control - feed forward correction?

Source reliability - (for  $\sim 100$  beams!)

Extra beams for reliability

Special operations - beam bending, splitting, combining

Electrical efficiency - special pulser circuits?

Magnet aberrations - emittance growth

Transverse/longitudinal coupling stable?

And more

All goes into an integrated end-to-end dynamical model.

# **LIA transport uses three types of focal elements**

Magnetic quadrupoles (HIF driver)

Electrostatic quadrupoles (MBE4, HIF driver?)

Solenoids (NDCX II, electron LIA, HIF driver?)

Other types of focusing exist but should be minimized in the accelerator:

- electron clouds

- higher order multipoles

- weak focusing from bends

- beam - beam interaction

- reflection from pipe surface

- image charge and current effects

- magnet fringe fields

Accel/Decel focusing is also always present and is important in injectors

All of this goes into a dynamical model



## Transport limit - simple model

$$\frac{d^2x}{dt^2} \approx \underbrace{-\omega_0^2 x}_{\text{Focal system}} + \underbrace{\frac{Ze}{\gamma M} (E_x - vB_y)}_{\text{Space charge}} \quad \text{single ion transverse motion}$$

$$\approx -\left( \omega_0^2 - \frac{Ze}{\gamma M} \frac{\rho}{2\epsilon_0 \gamma^2} \right) x$$

$$\rho \approx \frac{2\epsilon_0 \gamma^3 M}{Ze} \omega_0^2 \quad \text{for a very cold beam}$$

Large  $\rho$  is a good figure of merit but there are other considerations:

line charge density per beamlet

$$\lambda \approx \rho \pi a^2$$

Field limits, e.g.

$$B \leq 10T$$

$$E \leq 5\text{MV}/m$$

$$\Phi \leq 100kV$$

Stability: Phase advance per focal system period less than about  $80^\circ$

# Solenoid transport

In a reference frame rotating at the Larmor frequency ( $-\omega_c/2$ ):

$$\omega_0^2 = \left(\frac{\omega_c}{2}\right)^2 = \left(\frac{ZeB}{2\gamma M}\right)^2$$

$$\rho \approx \frac{2\varepsilon_0\gamma^3 M}{Ze} \left(\frac{ZeB}{2\gamma M}\right)^2 = \frac{\varepsilon_0}{2} \frac{Ze\gamma}{M} B^2$$

$$\lambda = \rho\pi a^2 = \left(10\frac{\mu C}{m}\right) \left(\frac{Z}{M/133amu}\right) \left(\frac{B}{10T}\right)^2 \left(\frac{a}{10cm}\right)^2$$

This looks pretty good for large radius beams at low energy ( $< 100\text{MeV}$ ), but it may not work for multiple beams.

**Magnetic quadrupoles** have a strong transverse field alternating in sign:

$$\vec{B} \approx \pm B' \quad (x\hat{e}_y + y\hat{e}_x)$$

For lattice period  $P$  with 50% magnet occupancy:

$$\omega_0^2 \approx \frac{P^2}{96} \left( \frac{Ze}{\gamma M} \right)^2 B'^2$$

$$\rho \approx \frac{\varepsilon_0}{48} \frac{Ze\gamma}{M} (P^2 B'^2)$$

Looks similar to solenoid but  $P$  can become large as ion energy increases. Superconducting pole fields (in wire) may reach about 6T:

$$B_{pole} \approx 2B'a \leq 6T$$

Beam channels in multibeam arrays can share poles in an efficient design.

**Electrostatic quadrupoles** seem similar to magnetic quadrupoles; just substitute

$$B' \longrightarrow E' / v \text{ transverse field gradient}$$

$$\rho \approx \frac{\epsilon_0}{48} \frac{Ze\gamma}{M} \frac{P^2 E'^2}{v^2} \quad (50\% \text{ occupancy})$$

But the pole potential is limited by the multibeam geometry and high voltage feeds:

$$\Phi_{Pole} \approx 2a^2 E' \leq 100kV$$

Combined with the stability condition line charge density per beamlet is limited:

$$\lambda \leq \frac{1}{2} \frac{\mu C}{m} \quad (\text{independent of } Z, M, v)$$

# Longitudinal dynamical models are not well developed for high current ion beams

Simple multibeam model equations:

$$I = \lambda v$$

$$\frac{\partial I}{\partial t} + \frac{\partial \lambda}{\partial z} = 0$$

$$\frac{\partial v}{\partial t} + v \frac{\partial v}{\partial z} = \frac{Ze}{\gamma^3 M} \left( E_0 + E_I - g \frac{\partial \lambda}{\partial z} \right)$$

The field induced by return current (-I) has been approximated using a circuit equation:

$$-E_I = RI + L \frac{\partial I}{\partial t} + \frac{1}{C} \int^t I(t') dt'$$

stabilizing

destabilizing

The space charge force  $\left( \sim \frac{\partial \lambda}{\partial z} \right)$  is stabilizing.

- At low frequencies ( $\sim 10 \text{ MHz}$ ) the circuit parameters are related to pulser design and electrical efficiency.
- High frequency values ( $\sim 100 \text{ MHz}$ ) may have different circuit parameters (module design).
- Unstable (e-fold) distances  $\sim 100 \text{ m}$  have previously been calculated. Feed-forward correction may be a solution.
- Spread  $\Delta P/P \sim 10^{-2}$  may stabilize but this is too large for final focus.
- Multiple beam effects probably important at high frequency.
- Other modes may be excited.
- Renewed study and a good pulser/module model are desirable.